

International Conference on Intelligent Robots and Systems
Detroit, Michigan USA | October 1, 2023



WORKSHOP: 08:30-17:30

ASSEMBLING LARGE INFRASTRUCTURES IN SPACE USING INTELLIGENT ROBOTS

ORGANIZED BY:

Craig Carignan
Mini Rai
Carol Martinez
Giacomo Marani

University of Maryland, USA
University of Lincoln, UK
University of Luxemburg
West Virginia Robotics Technology Center



<http://wvrtc.com/iros2023>

1

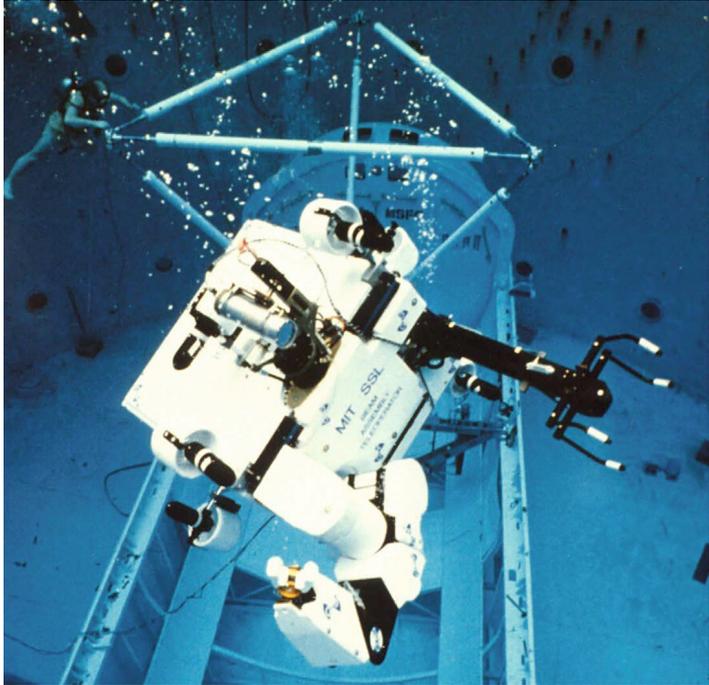
Robotic and Human/Robotic Structural Assembly: Past Experiences, Future Promise

David Akin

*University of Maryland
Space Systems Laboratory*

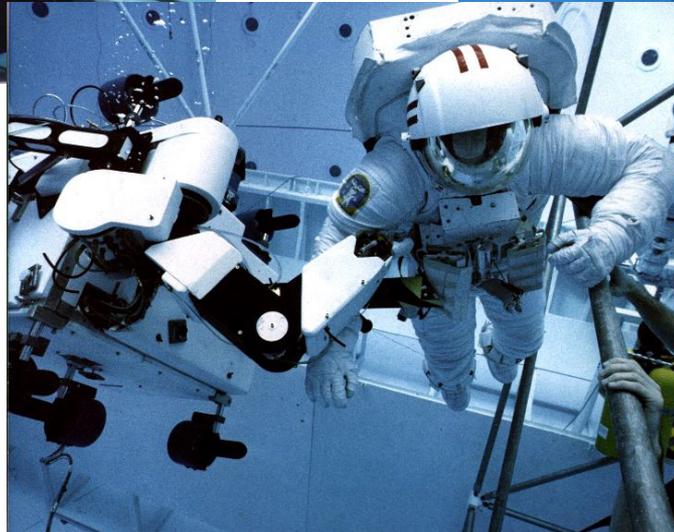
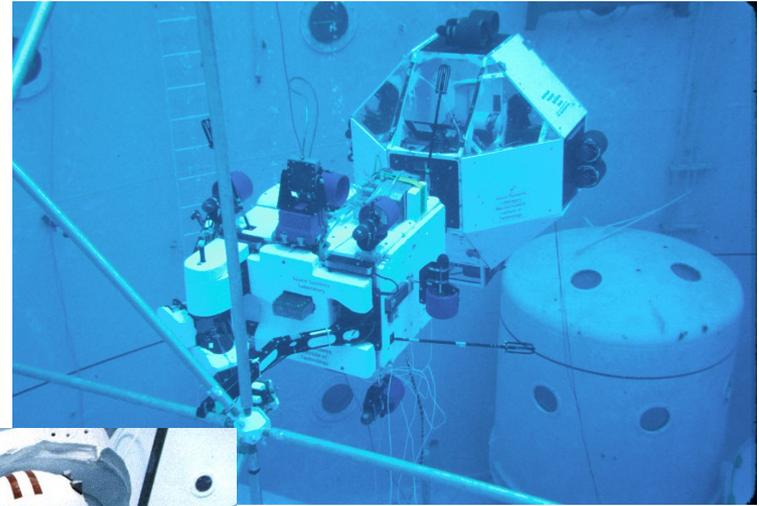
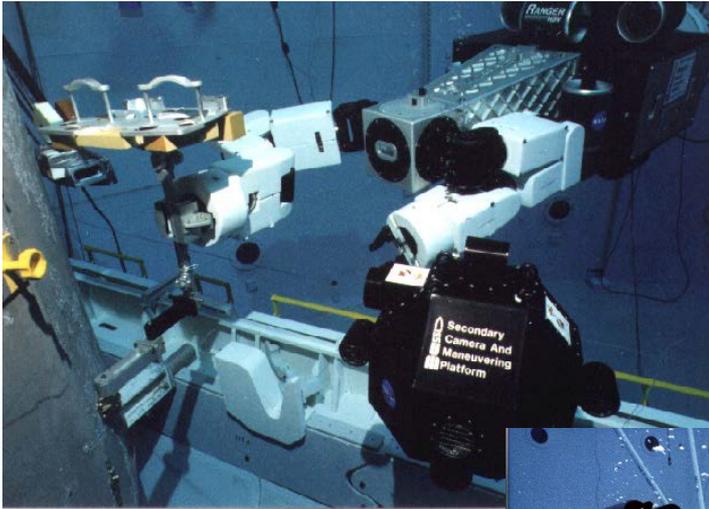


Experimental
Assembly of
Structures in EVA
(EASE) structure on
STS 61-B (1985)



Robotic Assembly of EASE and other structures in neutral buoyancy.

Multi-Agent Collaboration



Future Applications



Human-Robot Collaborative Manipulation of Deformable Objects for In-Space Assembly

Burak Aksoy

John T. Wen

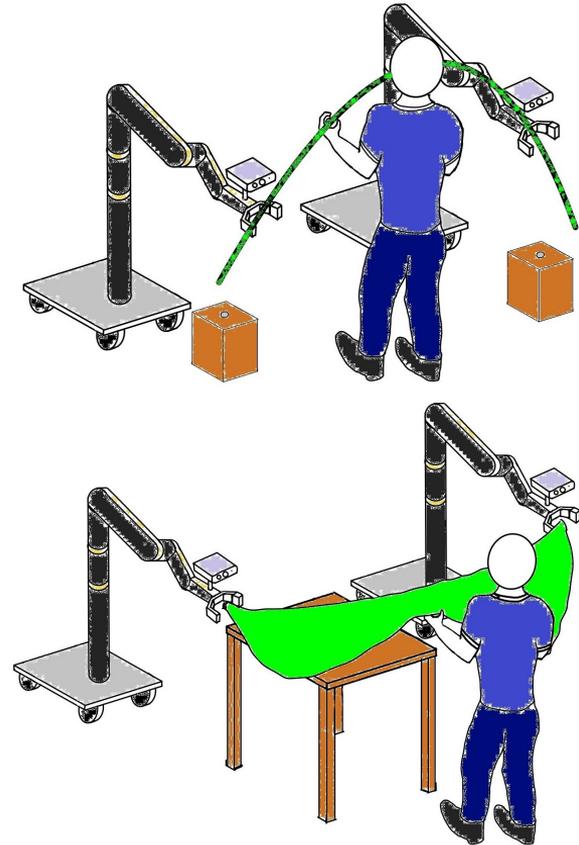


Rensselaer

why not change the world?®

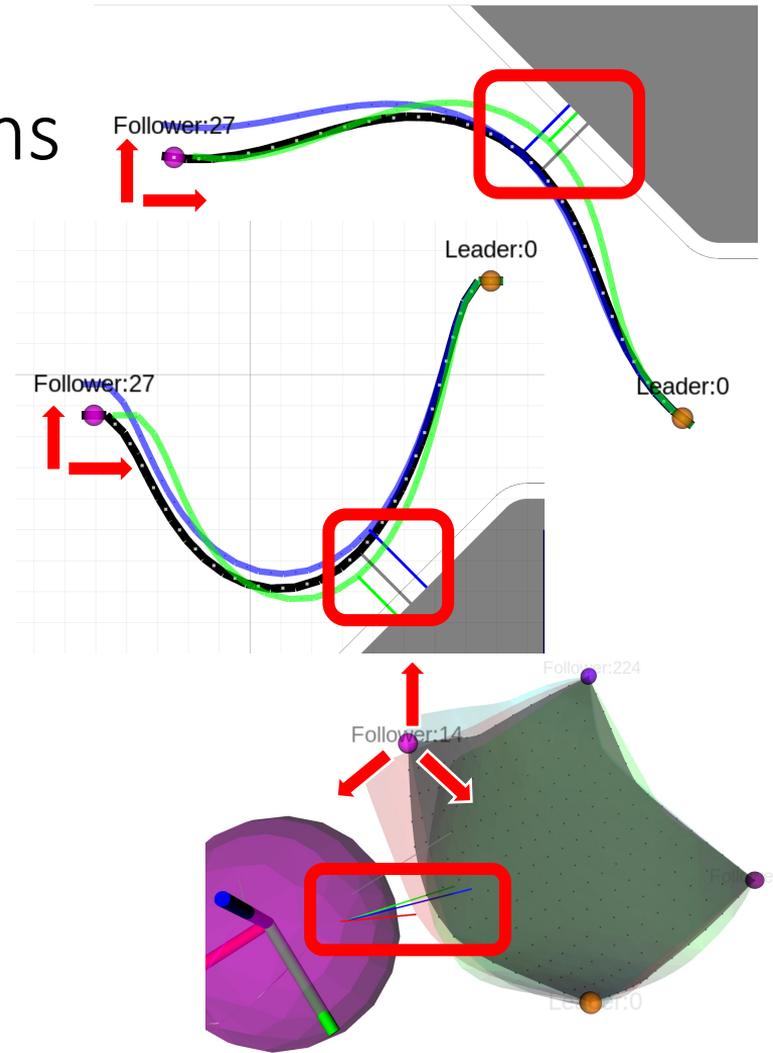
Collaboration for In-Space Assembly

- Focus:
 - Deployable booms & Flexible sheets
- Challenges in Deformable Object Manipulation
 - Modeling, Diversity, Variable Stiffness
- Human Limitations:
 - Fatigue & Error
- DOM Complexity:
 - Ensuring Safety in High DoF
- **Solution:**
Merge Human Intelligence & Robotic Assistance
 - Human Focus: Precision;
 - Robots: Prediction & Adjustment



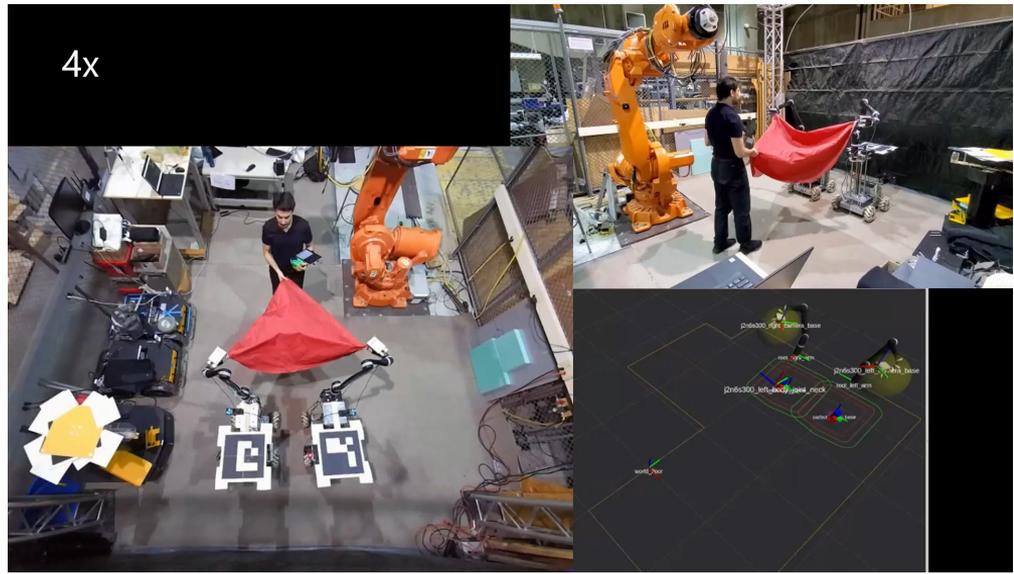
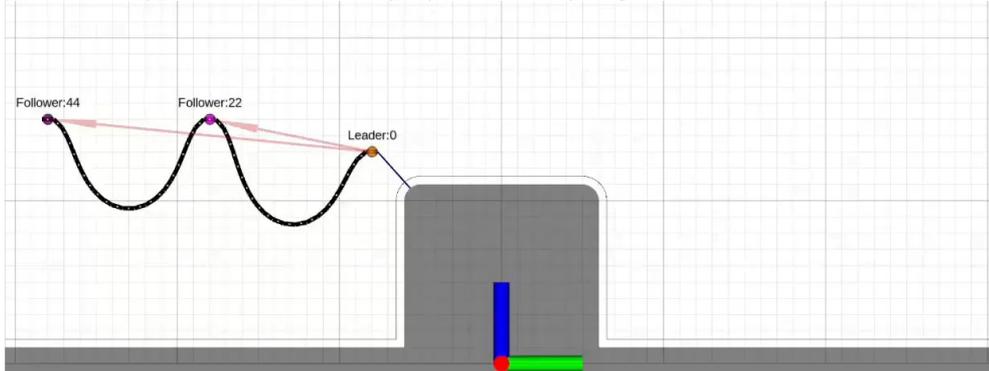
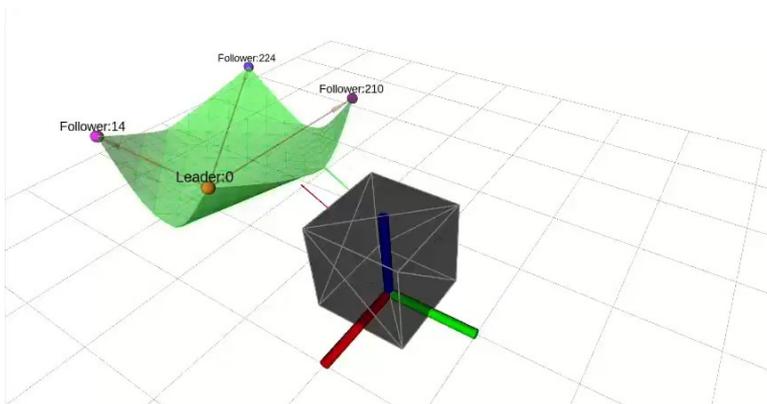
Methodology & Contributions

- Real-time Flexible Material Simulation
 - With Position-Based Dynamics (PBD) & ROS
- Safety:
 - Control Barrier Functions
 - Prevents Overstretching & Collisions
- Versatile:
 - 1D Beams/ropes & 2D Fabrics
- Input:
 - Human Position Tracking
 - Depth sensor
 - F/T sensors



Demonstrations

- Both Simulated & Real-world



3

Effect of Orbital Dynamics on Fuel Use in Sampling-based Plans for Proximity Operations

Brandon Apodaca¹, Ella Atkins², Leia Stirling¹

¹University of Michigan, ²Virginia Tech

Introduction and Background

- There is a need for free-flyer inspections on the International Space Station [1].
- Motion planners for space proximity operations effectively **minimize costs** associated with orbital dynamics, however they struggle to optimize paths with **complex obstacle fields** [2,3].
- Robotics path planners are effective at **obstacle avoidance**, however they do not account for **orbital dynamics** [4,5].

[1] R. Moore, "ISS Inspection Capabilities and Challenges," presented at the In-Space Inspection Workshop, NASA Johnson Space Center, Jul. 2014. Accessed: May 17, 2023. [Online]. Available: <https://mediaex-server.larc.nasa.gov/Academy/Play/09e01da677ed4f768d6d9f020e3fa4ec1d>

[2] K. Berry et al., "OSIRIS-REX Touch-And-Go (TAG) Mission Design and Analysis," presented at the 36th Annual AAS Guidance and Control Conference, Breckenridge, CO, Feb. 2013. Accessed: May 09, 2023. [Online]. Available: <https://ntrs.nasa.gov/citations/20130013409>

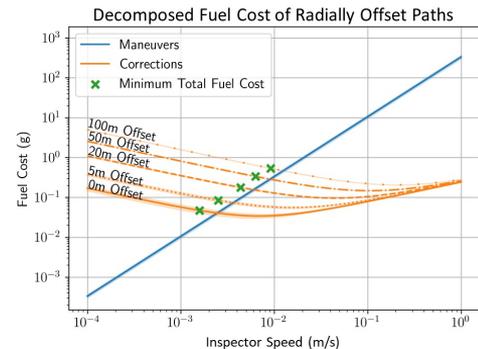
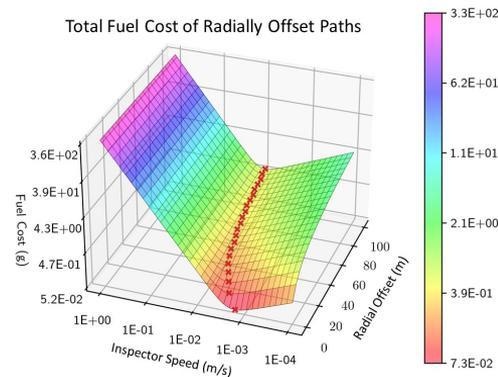
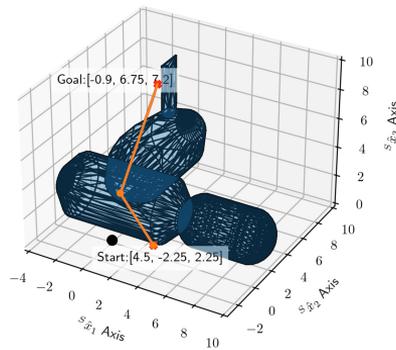
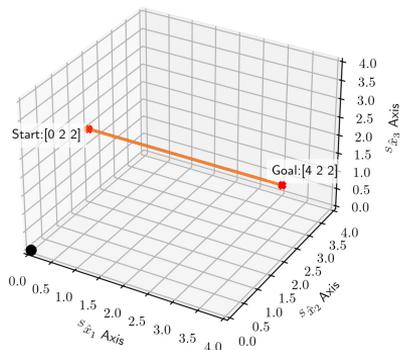
[3] M. Pyrak and J. Anderson, "Performance of Northrop Grumman's Mission Extension Vehicle (MEV) RPO imagers at GEO," in *Autonomous Systems: Sensors, Processing and Security for Ground, Air, Sea and Space Vehicles and Infrastructure 2022*, M. C. Dudzik, T. J. Axenson, and S. M. Jameson, Eds., Orlando, United States: SPIE, Jun. 2022, p. 28. doi: 10.1117/12.2631524.

[4] S. M. LaValle, "Rapidly-exploring random trees: A new tool for path planning," Computer Science Department, Iowa State University, Technical Report TR 98-11, Oct. 1998. [Online]. Available: <http://msl.cs.uiuc.edu/~lavalle/papers/Lav98c.pdf>

[5] B. Apodaca, E. Atkins, and L. Stirling, "RRTZ: a Path Planner Designed for Zero Gravity," IEEE Aerospace Conference, 2024, In press.

Methods and Results

- Robotics planner RRTZ [5] was used to produce continuous trajectories on four different obstacle fields (two below).
- We leveraged Newtonian mechanics to estimate fuel cost using the Clohessy Wiltshire Equations [6] (right).



[5] B. Apodaca, E. Atkins, and L. Stirling, "RRTZ: a Path Planner Designed for Zero Gravity," IEEE Aerospace Conference, 2024, In press.

[6] W. H. Clohessy and R. S. Wiltshire, "Terminal Guidance System for Satellite Rendezvous," Journal of the Aerospace Sciences, vol. 27, no. 9, pp. 653–658, Sep. 1960, doi: 10.2514/8.8704.



STAARK Robotic Arm system

- System Overview

Scalable in-space robotics



SCALABLE AND MODULAR

- Customizable DOF
- Select best configuration & reach
- Adjust for optimal loads transfer
- New features can be installed

OPTIMIZED

- Integrated avionics
- Easily programmable software
- Lightweight components
- High performing systems

VISION-GUIDED ROBOTICS

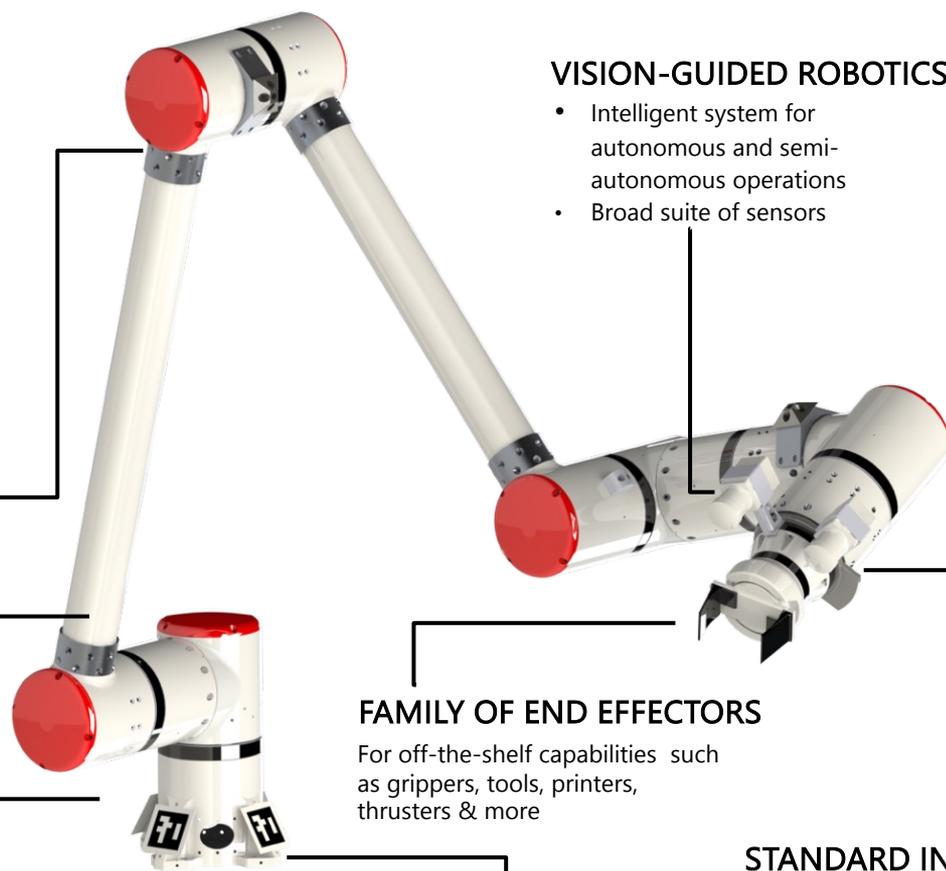
- Intelligent system for autonomous and semi-autonomous operations
- Broad suite of sensors

FAMILY OF END EFFECTORS

For off-the-shelf capabilities such as grippers, tools, printers, thrusters & more

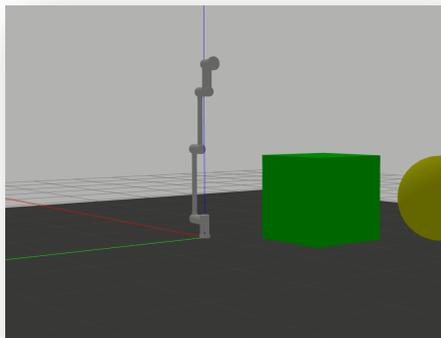
STANDARD INTERFACES

Integration with spacecraft and connecting custom end-effectors

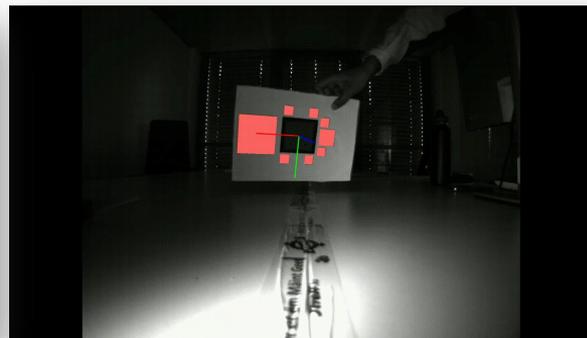


Robotics Functions & Capabilities

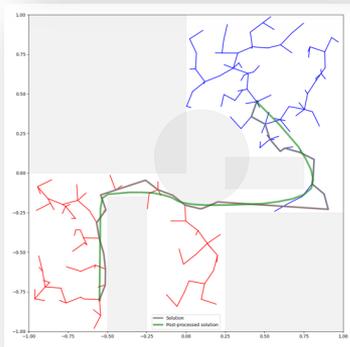
- STAARK 6–DoF allows for a fully reachable dome-type workspace that allows for complex operations and trajectories
- **Robotic System equipped with MACOS (Manipulator Control Stack):**
 - Running onboard the RCU.
 - As a simulation instance on the ground station.
- **Robotics Capabilities include:**
 - Joint Space Control
 - Cartesian Pose Control
 - Static Environment Collision Detection
 - Static Environment Path Planning
 - Tool Based Operations Planning (static offset from tool flange)
 - Compliance Control (Coming 2024)
 - Visual servoing (Coming 2024)



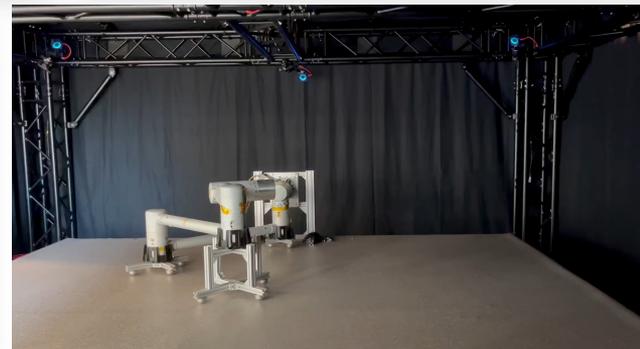
Collision Detection



Fiducial Marker Identification



Path Planning



Control

5 Efficient and Singularity-Aware Inverse Kinematics for 6-DOF and 7-DOF Revolute Manipulators



Alexander J. Elias and John T. Wen · Rensselaer Polytechnic Institute

Slide 2: Canonical Subproblems for Robot Inverse Kinematics [1]

Slide 3: General, Conventional, and Stereographic SEW Angles for 7-DOF Arms [2]

Slide 4: 6-DOF and 7-DOF IK using Subproblem Decomposition Method [1, 2]



linktr.ee/iros_ik
eliasa3@rpi.edu
github.com/rpiRobotics/ik-geo
github.com/rpiRobotics/stereo-sew



OSAM-1 (2R-2R-3R)



OSAM-2 (R-2R-2R-2R)



SSRMS (2R-3R||-2R)



RRC (General 7R)

[1] Alexander J. Elias and John T. Wen, "Canonical subproblems for robot inverse kinematics," *arXiv preprint arXiv:2211.05737*, 2022

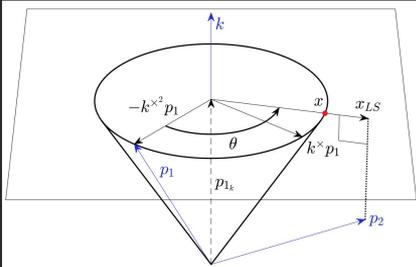
[2] —, "Redundancy parameterization and inverse kinematics of 7-DOF revolute manipulators," *arXiv preprint arXiv:2307.13122*, 2023

Canonical Subproblems for Robot Inverse Kinematics

Angle of intersection of circles with other geometric objects

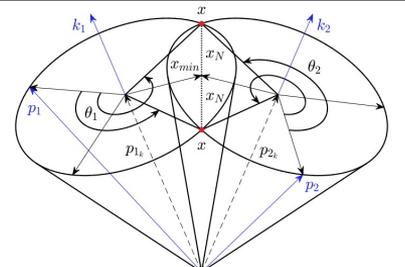
Least-squares (1–4) and detect/resolve continuum of solutions

1: Circle and Point



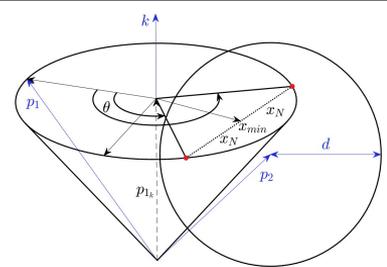
$$\min \|R(k, \theta)p_1 - p_2\|$$

2: Two Circles



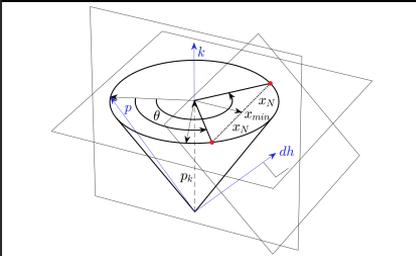
$$\min \|R(k_1, \theta_1)p_1 - R(k_2, \theta_2)p_2\|$$

3: Circle and Sphere



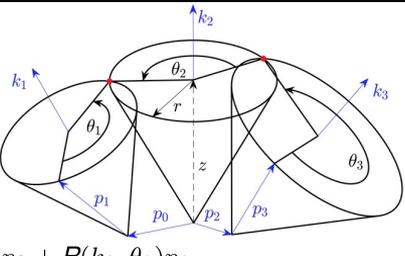
$$\min \| \|R(k, \theta)p_1 - p_2\| - d\|$$

4: Circle and Plane



$$\min |h^T R(k, \theta)p - d|$$

5: Three Circles



$$p_0 + R(k_1, \theta_1)p_1 = R(k_2, \theta_2)(p_2 + R(k_3, \theta_3)p_3)$$

6: Four Circles

$$\begin{cases} h_1^T R(k_1, \theta_1)p_1 + h_2^T R(k_2, \theta_2)p_2 = d_1 \\ h_3^T R(k_3, \theta_1)p_3 + h_4^T R(k_4, \theta_2)p_4 = d_2 \end{cases}$$

Solution method:

1. Write in terms of $x = \begin{bmatrix} \sin \theta \\ \cos \theta \end{bmatrix}$
2. Find unconstrained solutions
3. Add $\|x\| = 1$ constraint
4. Return $\theta = \text{atan2}(\sin \theta, \cos \theta)$

No arccos, arcsin, or $\tan(\theta/2)$
 → Robust to numerical issues

Solutions are fast with MATLAB and Rust

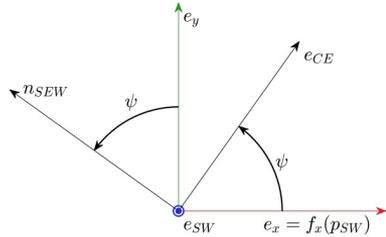
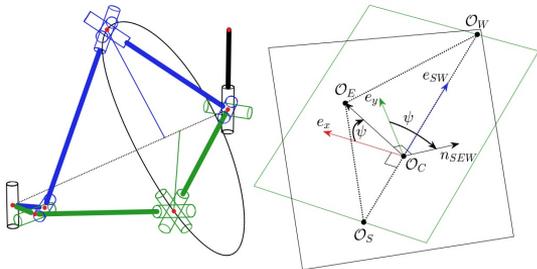
Subproblem	Mean Runtime (ns)		
	m-file	MEX	Rust
1: Circle and Point	13 517	36	59
2: Two Circles	27 262	312	242
3: Circle and Sphere	18 034	134	111
4: Circle and Plane	17 669	105	115
5: Three Circles	105 288	2 553	1 027
6: Four Circles	116 750	3 110	1 436

General, Conventional, and Stereographic SEW Angles for 7-DOF Arms

Shoulder-Elbow-Wrist (SEW) angle parameterizes redundant DOF

General SEW Angle

Parameterization with arbitrary reference direction function $e_x = f_x(p_{SW})$

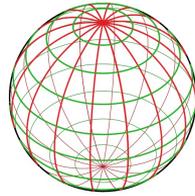
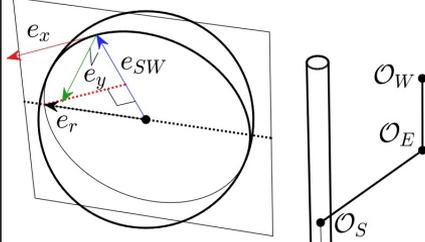


$$\psi = \arg \min_{\theta} \|R(e_{SW}, \theta)e_x - p_{SE}\|$$

$$n_{SEW} = R(e_{SW}, \psi)e_y$$

Conventional SEW Angle

Singularity if wrist on line
May limit usable workspace



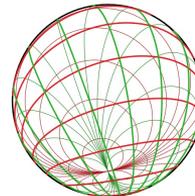
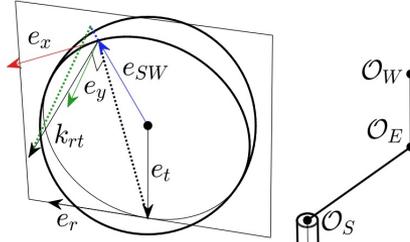
$$e_x = f_x(p_{SW}) = e_y^{\times} e_{SW},$$

$$e_y = \frac{k_y}{\|k_y\|},$$

$$k_y = p_{SW}^{\times} e_r.$$

Stereographic SEW Angle

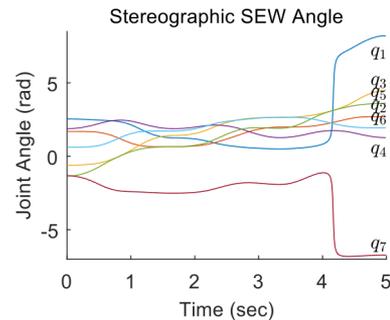
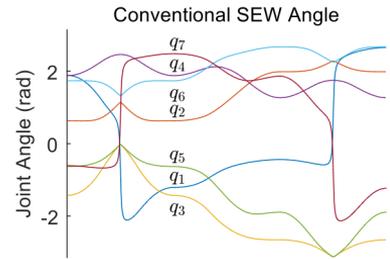
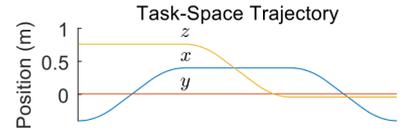
Singularity if wrist on half-line
Singularity can be out of reach



$$e_x = f_x(p_{SW}) = \frac{k_x}{\|k_x\|},$$

$$k_x = k_{rt}^{\times} p_{SW},$$

$$k_{rt} = (e_{SW} - e_t)^{\times} e_r.$$



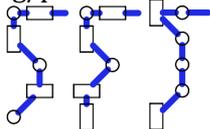
6-DOF and 7-DOF IK using Subproblems Decomposition Method

Finds all solutions

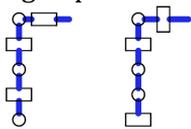
Robust to internal and boundary singularities

6-DOF Inverse Kinematics

3 intersecting/parallel axes: Closed form

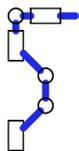


2 intersecting or parallel axes: 1D search

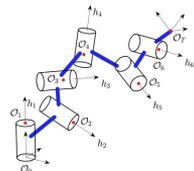


Example: Spherical wrist & two parallel axes

1. Find q_1 with SP 4
2. Find q_3 with SP 3
3. Find q_2 with SP 1
4. Find (q_4, q_5) with SP 2
5. Find q_6 with SP 1

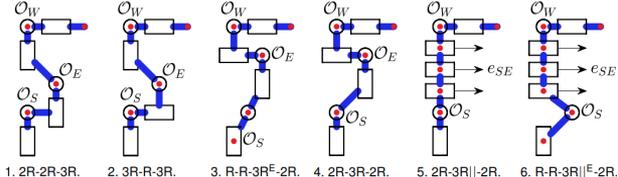


General 6R robot: 2D search



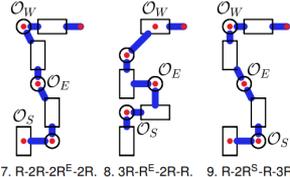
7-DOF Inverse Kinematics (Using General SEW Angle)

Closed form:



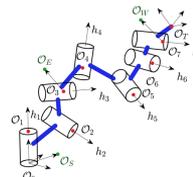
1. 2R-2R-3R.
2. 3R-R-3R.
3. R-R-3R^E-2R.
4. 2R-3R-2R.
5. 2R-3R||-2R.
6. R-R-3R||^E-2R.

1D search:



7. R-2R-2R^E-2R.
8. 3R-R^E-2R-R.
9. R-2R^S-R-3R.

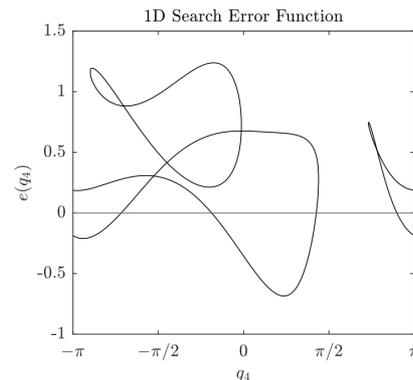
General 7R robot: 2D Search



Subproblem decomposition is faster and more capable than IKFast and MATLAB Robotics Toolbox (Pieper method)

Robot Type	Mean Hardcoded Robot Runtime (μ s)			
	MEX	Rust	IKFast	MRT MEX
General 6R (2D search)	20 741.535	16 026.010	N/A ^a	N/A ^a
Two intersecting axes (1D search)	199.194	114.552	N/A ^a	N/A ^a
Two parallel axes (1D search)	1 021.655	439.445	N/A ^a	N/A ^a
Spherical wrist	4.527	2.425	111.445	10.583
and two intersecting axes	4.991	3.688	N/A ^b	N/A ^a
and two parallel axes	2.991	3.183	4.417	13.318
Three parallel axes	5.345	4.339	N/A ^c	N/A ^a
and two intersecting axes	2.846	3.089	121.714	N/A ^a

^a Did not generate code ^b Did not compile ^c Incorrect IK





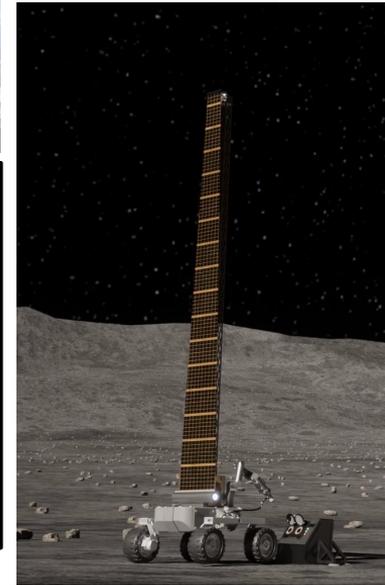
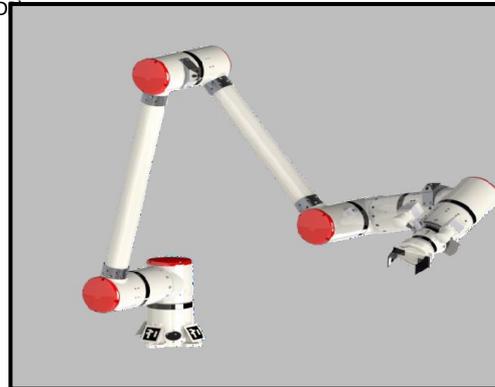
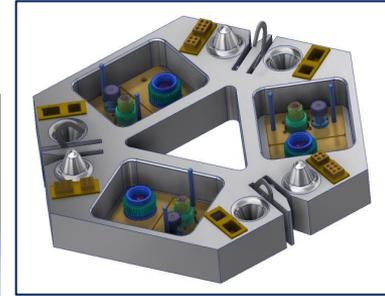
OSAM-2 Technologies for Autonomous Construction of Large Structures on Orbit

Dr. Daniel Hillsberry 10.01.23

OSAM-2 Technologies for Autonomous Construction of Large Structures on Orbit

On the NASA OSAM-2 program, Redwire developed unique technologies required to construct additively manufactured structures on orbit at scales of 10s of meters on orbit:

- Extended Structure Additive Manufacturing Machine (ESAMM)
 - Leverages development from Additive Manufacturing Facility (AMF) and 3D Printing in Zero G (3DP)
 - Belongs to Redwire family of technologies for large structures into the open volume of space
 - Smaller parts like rover wheels on the surface of the Moon
 - Redwire's robotic control algorithms running on computationally limited flight hardware
 - Enable precision manipulation
 - In-situ inspection
 - Safely interact and grasp components using compliance control
 - Precision movements with visual servoing,
 - Avoid undesirable configurations autonomously.
 - Redwire modeled, simulated, and analyzed robotically constructed large structures
 - Simulation run on all phases of build through changing structural dynamics
 - Developed techniques to prevent excitation of low frequency structural modes
 - Developed structural monitoring and control systems
- This poster discusses these methods and terrestrial tests in the context of mission requirements.



Enabling Technologies

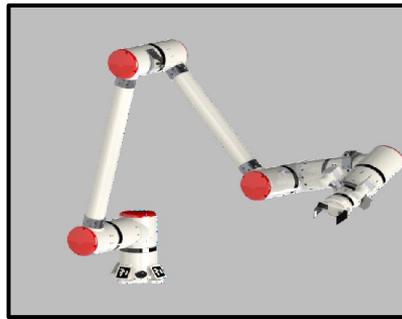
End Effector



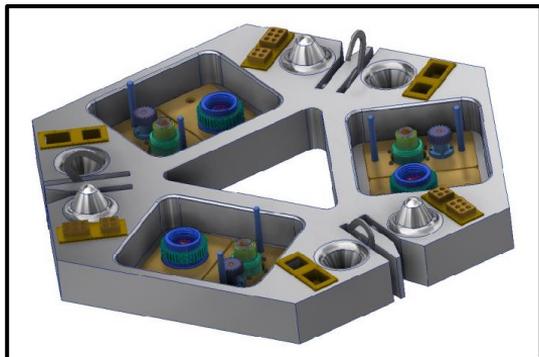
Standard Interface



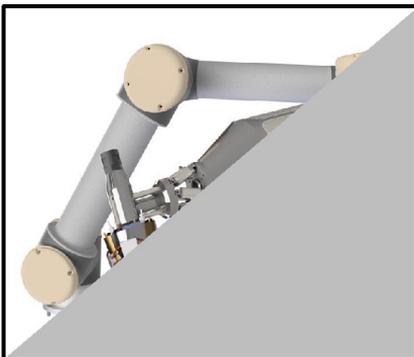
Robotics



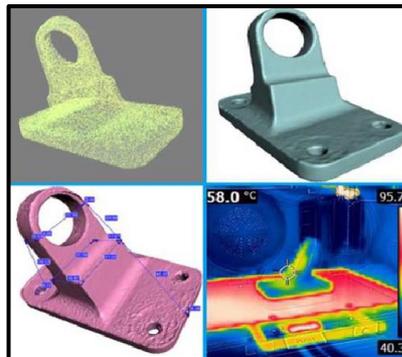
Structures



Standard Interface



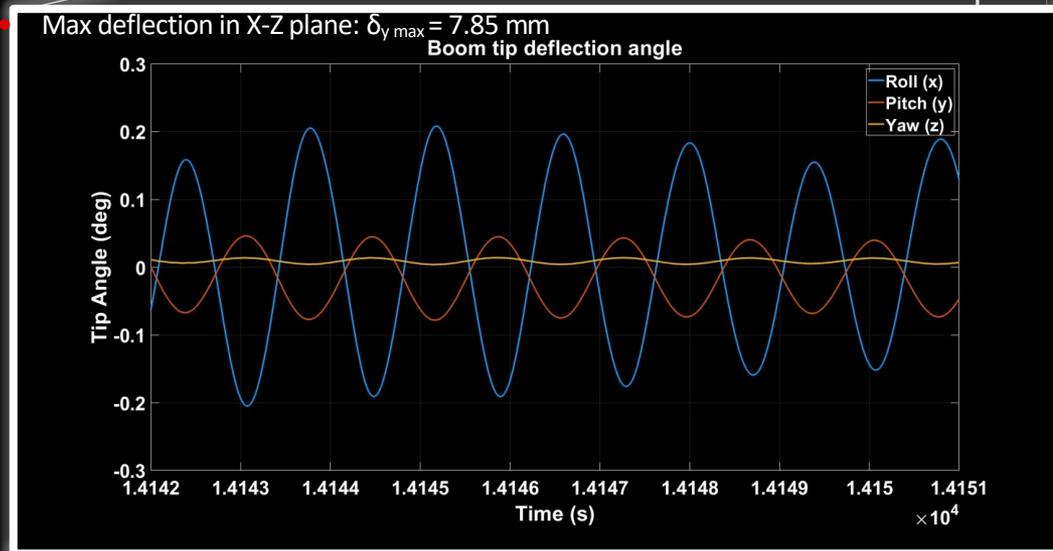
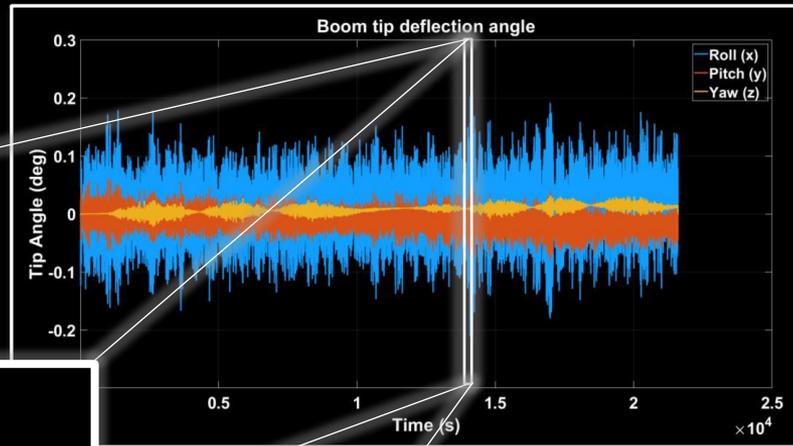
Autonomy



In Situ Inspection

SSM Results: Beam Deflection

- Comparing the boom tip angles to the SV angles shows how the boom is deflecting with respect to the SV
- The largest deflection occurs around the X axis, or in the Y-Z plane, which matches the highest torque generated by the gantry moving along the Y axis
- Max deflection in Y-Z plane: $\delta_{x \max} = 27.5 \text{ mm}$



Distributed Load $w = \frac{\theta_{\max} * 6 * E * I}{L^3}$

Deflection $\delta_{\max} = \frac{w * L^4}{8 * E * I}$

Moment $M_{\max} = \frac{-w * L^2}{2}$

Stress $\sigma_{\max} = \frac{M * y}{I}$

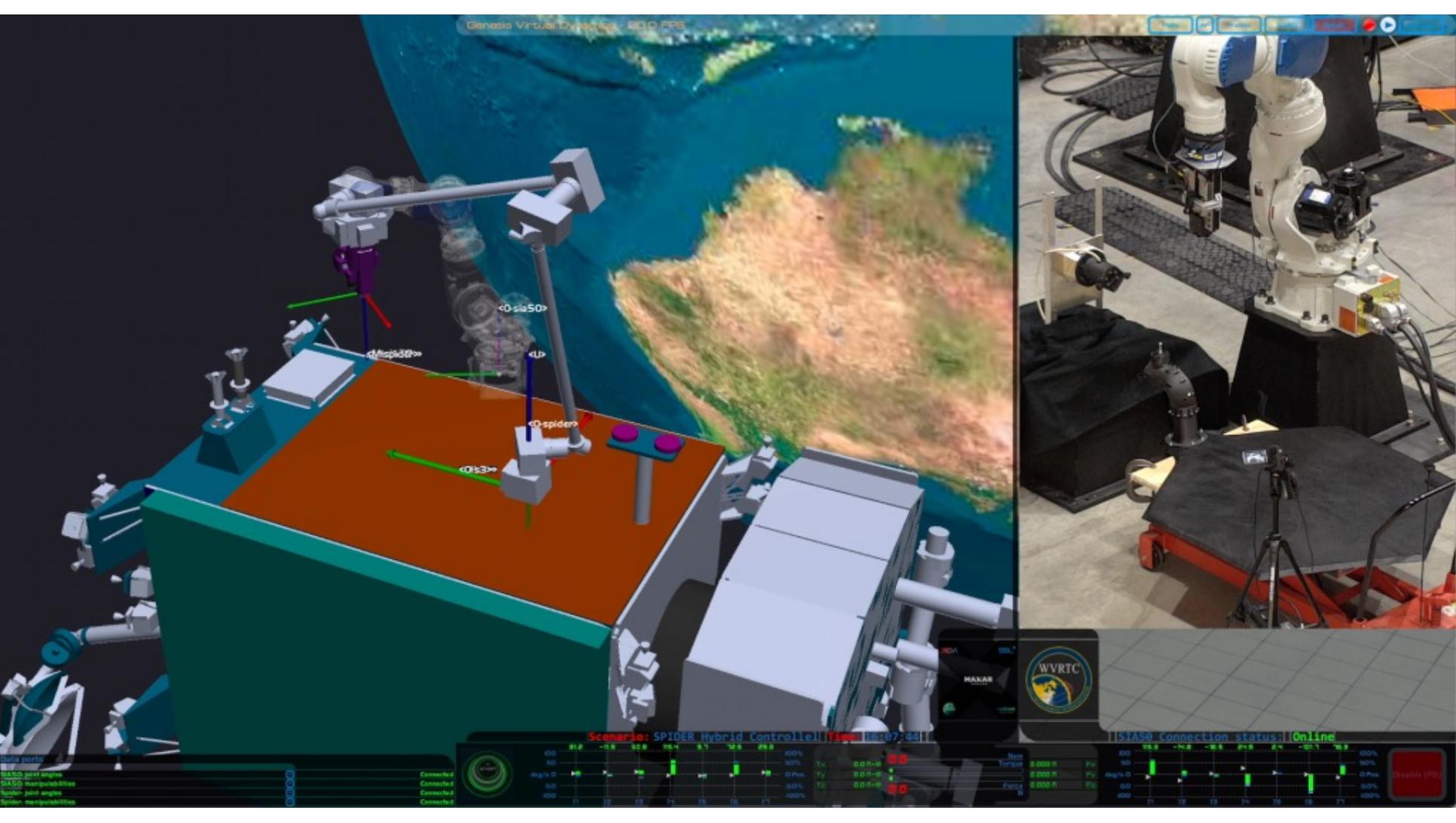
Hardware-in-the-loop simulation of modular antenna assembly

Alycia Gailey

Giacomo Marani

West Virginia Robotic Technology Center

Robots are playing an increasing role in space exploration and in-space servicing. Robot arms are good for performing in-space tasks such as modular antenna assembly. The SPIDER arm (SPace Infrastructure Dexterous Robot) can perform assembly tasks in environmental conditions that would be dangerous for astronauts. Our work involves proof-of-principle testing of robot control systems on the ground using a hardware-in-the-loop (HIL) simulator, which simulates how the SPIDER robot end effector would move in space in response to externally applied forces from its environment. Using the HIL, we can test various robot control algorithms in a 1-G environment to see how well the robot system performs the different tasks that it would need to do in space.



8

Adaptive Framework for Convergent Manufacturing with Robot Manipulators

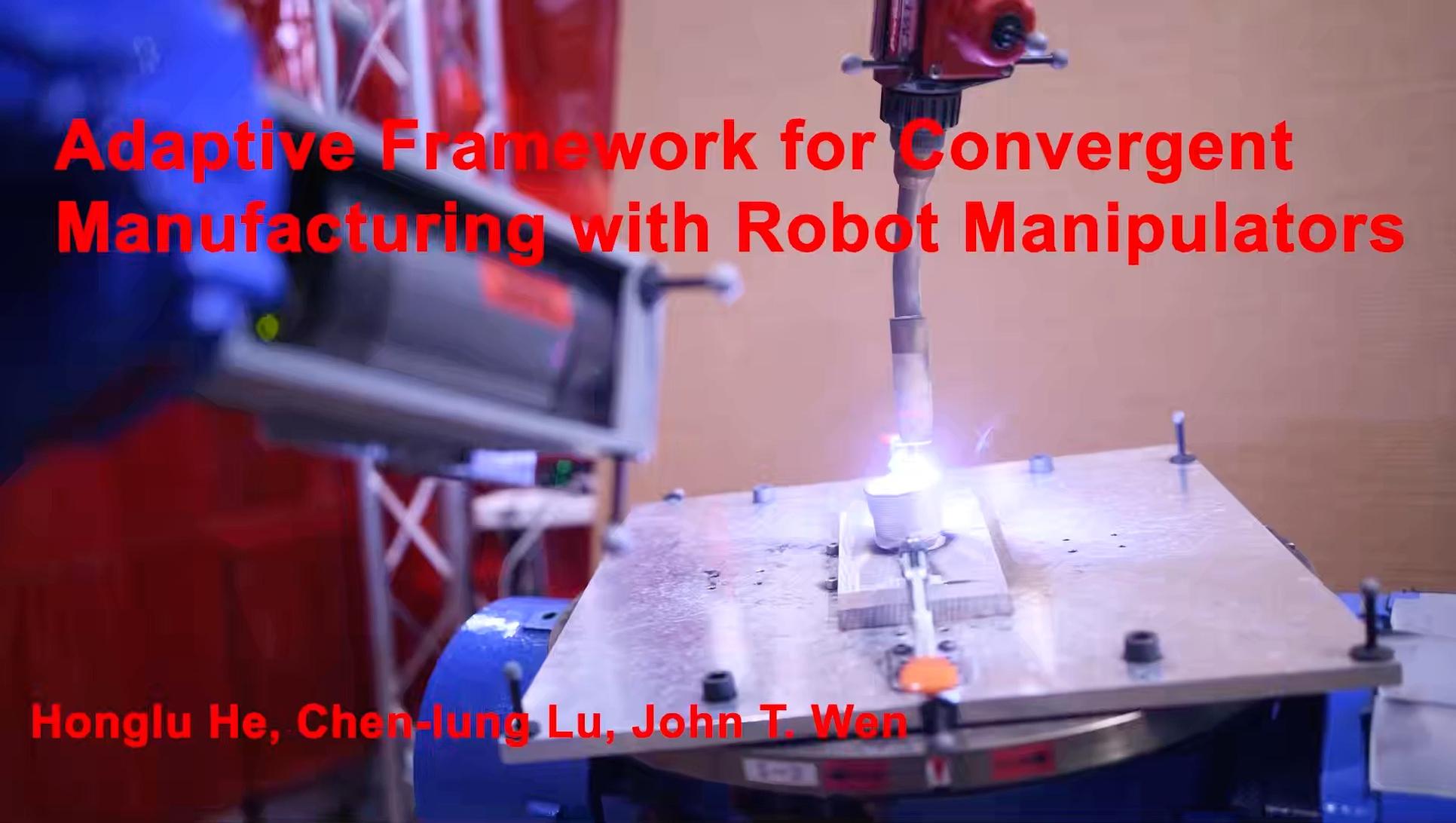
Honglu He

Chen-lung Lu

John T. Wen

Rensselaer Polytechnic Institute

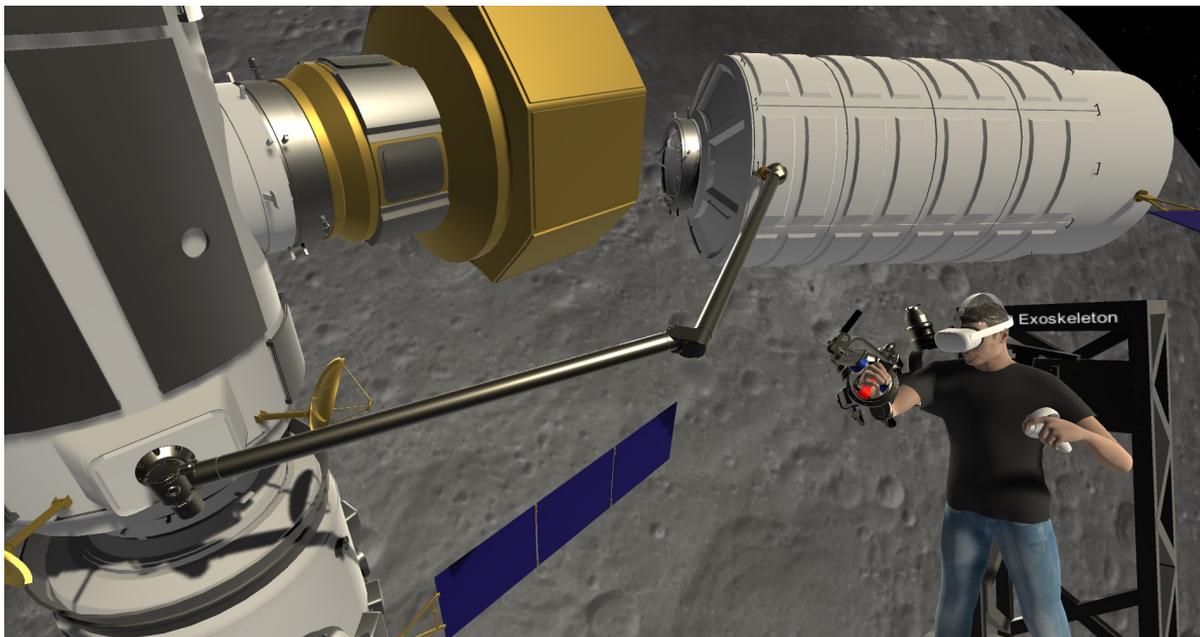


A close-up photograph of a robotic arm in a factory environment. The arm is positioned over a large, flat metal plate. A bright, intense light is emanating from the tip of the arm, suggesting a welding or laser cutting process. The background is slightly blurred, showing industrial structures and a red wall. The overall scene is lit with a mix of blue and red tones.

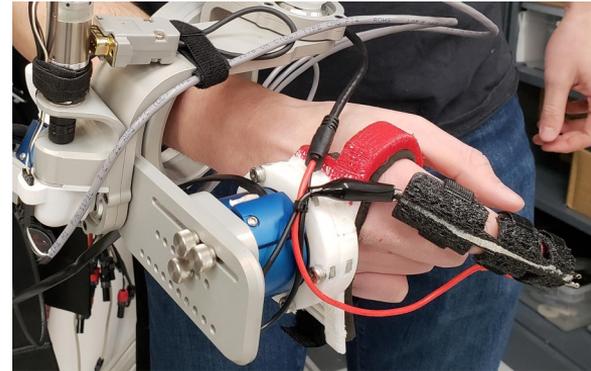
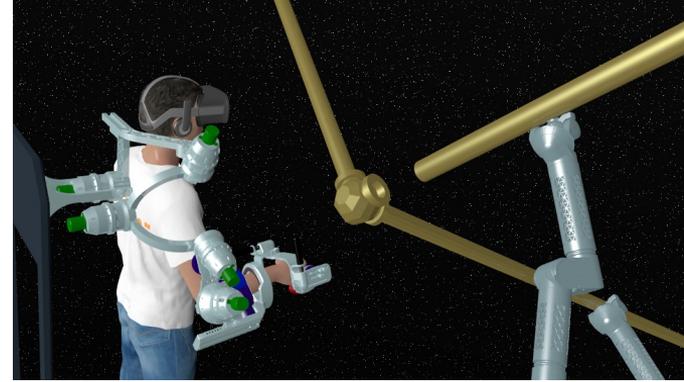
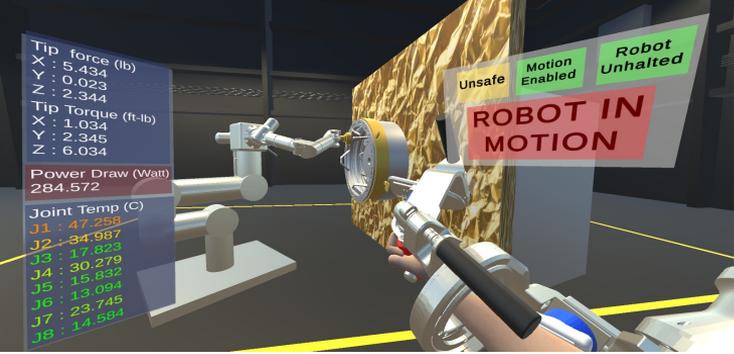
Adaptive Framework for Convergent Manufacturing with Robot Manipulators

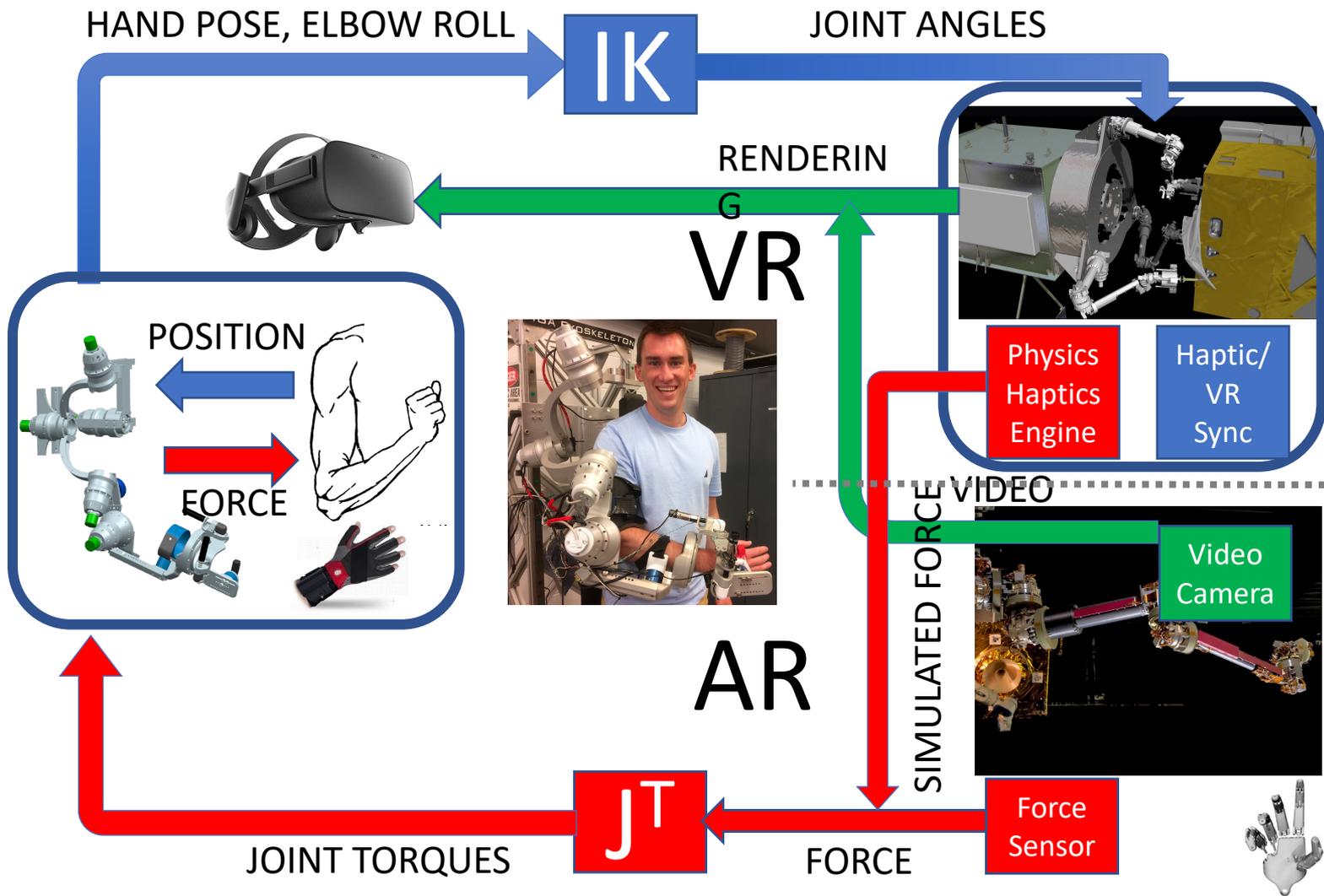
Honglu He, Chen-lung Lu, John T. Wen

Telerobotic Assembly of Structures in Space using an Exoskeleton-XR Interface



Romeo Perlstein, Daniil Gribook, Craig Carignan
University of Maryland



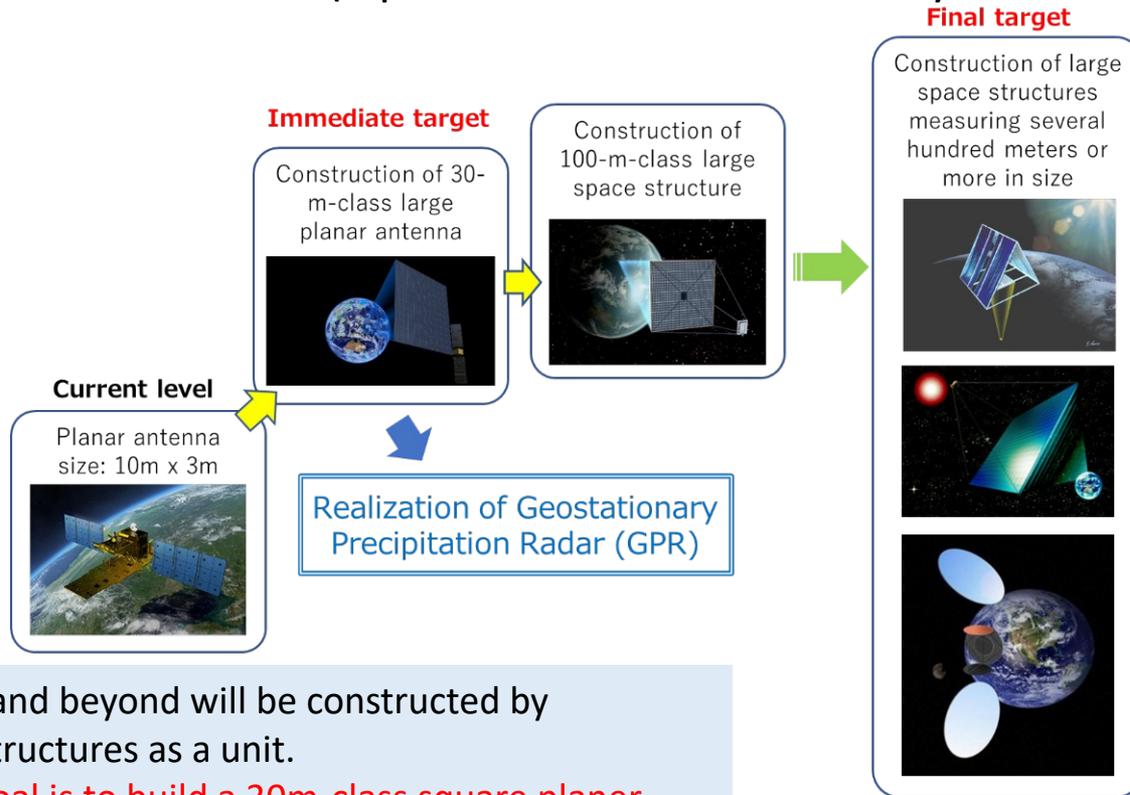


Deployable Lightweight Planar Antenna Technology Demonstration Mission

Keisuke WATANABE and Daisuke JODOI
Japan Aerospace Exploration Agency (JAXA)

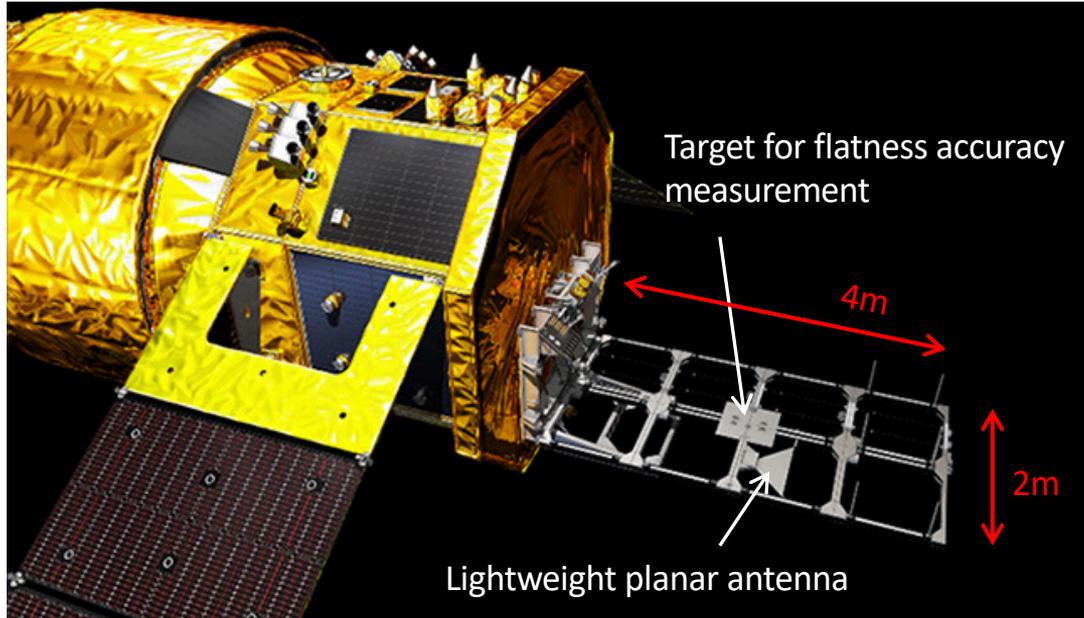


Steps toward the SSPS (Space Solar Power Systems)



- 100m-class structures and beyond will be constructed by combining 30m-class structures as a unit.
- **Our current research goal is to build a 30m-class square planer antenna.**

DELIGHT

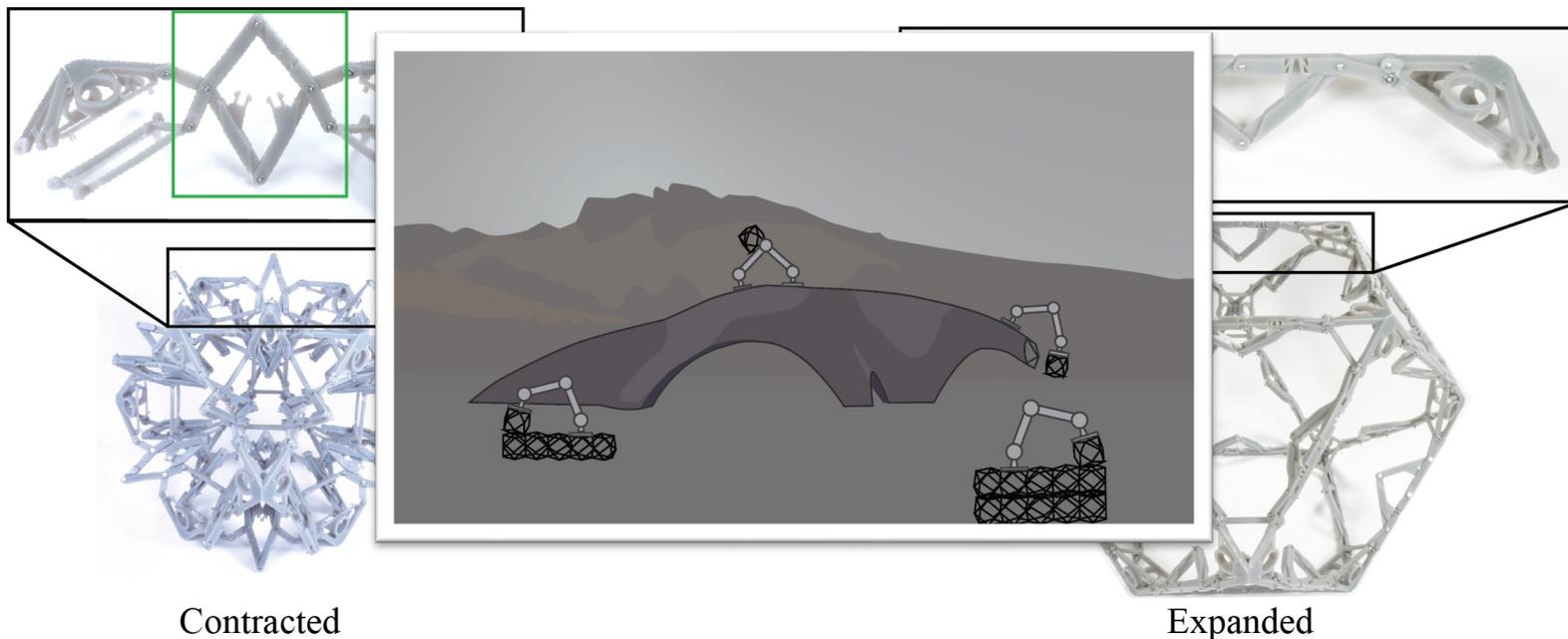


- Eight panels with deployment and connection mechanisms will be deployed row by row.
- Lightweight planar antenna will receive radio waves transmitted from the ground station.
- Dynamic behavior/flatness accuracy of the panels during/after deployment will be measured using cameras.

Expanding subunits for deep space infrastructure

Stephanie Woodman¹, Alex Moore¹, Kenneth Cheung², and Rebecca Kramer-Bottiglio¹

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Principles of Hoberman sphere optimized for our shape

